

Quartic Force Field Training

Brent R. Westbrook

Fortenberry Patch

What is a quartic force field?

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The obvious

$$F = ma$$

What is a quartic force field?

The obvious

$$F = ma$$

The more useful

$$F = -\nabla V = -\left(\frac{\partial V}{\partial x}, \frac{\partial V}{\partial y}, \frac{\partial V}{\partial z}\right)$$

How does this relate to us?

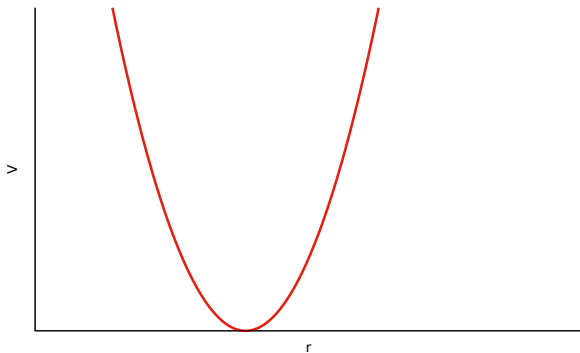
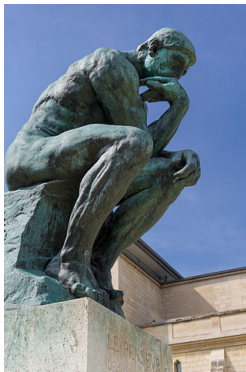


Figure: Potential vs displacement for a 1-D harmonic oscillator

How does this relate to us?

Suppose we do not know the potential energy function for a molecule. How could we approximate it?



How does this relate to us?

Taylor series

Definition

An infinite sum of terms that are expressed in terms of the function's derivatives at a single point, a

$$f(x)_a \approx f(a) + \frac{f'(a)}{1!}(x-a) + \frac{f''(a)}{2!}(x-a)^2 + \dots$$

Example

$$e^x_{a=0} \approx \frac{e^0}{0!} + \frac{e^0}{1!}(x-0) + \frac{e^0}{2!}(x-0)^2 + \dots = 1 + x + \frac{x^2}{2} + \dots$$

What is a quartic force field?

You've probably seen this in all of our papers:

Definition

A quartic force field is a fourth-order Taylor series expansion of the potential energy portion of the internuclear Watson Hamiltonian

And this in some of them:

Equation

$$V = \frac{1}{2} \sum_{ij} F_{ij} \Delta_i \Delta_j + \frac{1}{6} \sum_{ijk} F_{ijk} \Delta_i \Delta_j \Delta_k + \frac{1}{24} \sum_{ijkl} F_{ijkl} \Delta_i \Delta_j \Delta_k \Delta_l$$

Where did Taylor go?

Let's expand the potential energy for the 1-D harmonic oscillator, $V(r)$, about its equilibrium displacement r_{eq} , and let this be equal to zero.

$$V(r)_{r_{eq}} \approx \frac{1}{0!} V(r_{eq}) + \frac{1}{1!} \left(\frac{dV}{dr} \right)_{r_{eq}} (r - r_{eq}) + \frac{1}{2!} \left(\frac{d^2V}{dr^2} \right)_{r_{eq}} (r - r_{eq})^2 + \frac{1}{3!} \left(\frac{d^3V}{dr^3} \right)_{r_{eq}} (r - r_{eq})^3 + \frac{1}{4!} \left(\frac{d^4V}{dr^4} \right)_{r_{eq}} (r - r_{eq})^4$$

What do we know about the first two of these terms?

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$$\begin{aligned} V(r)_{r_{eq}} \approx & \frac{1}{0!} \cancel{V(r_{eq})} + \frac{1}{1!} \left(\frac{dV}{dr} \right)_{r_{eq}} (r - r_{eq}) + \frac{1}{2!} \left(\frac{d^2V}{dr^2} \right)_{r_{eq}} (r - r_{eq})^2 \\ & + \frac{1}{3!} \left(\frac{d^3V}{dr^3} \right)_{r_{eq}} (r - r_{eq})^3 + \frac{1}{4!} \left(\frac{d^4V}{dr^4} \right)_{r_{eq}} (r - r_{eq})^4 \end{aligned}$$

What do we know about the first two of these terms?

- ▶ The first cancels because we defined r_{eq} as our zero of potential

Where did Taylor go?

This leaves us with

$$\begin{aligned} V(r)_{r_{eq}} \approx & \frac{1}{2!} \left(\frac{d^2 V}{dr^2} \right)_{r_{eq}} (r - r_{eq})^2 \\ & + \frac{1}{3!} \left(\frac{d^3 V}{dr^3} \right)_{r_{eq}} (r - r_{eq})^3 \\ & + \frac{1}{4!} \left(\frac{d^4 V}{dr^4} \right)_{r_{eq}} (r - r_{eq})^4 \end{aligned}$$

which should be looking vaguely familiar

Where did Taylor go?

This leaves us with

$$\begin{aligned}
 V(r)_{r_{eq}} \approx & \frac{1}{2!} \left(\frac{d^2 V}{dr^2} \right)_{r_{eq}} (r - r_{eq})^2 \\
 & + \frac{1}{3!} \left(\frac{d^3 V}{dr^3} \right)_{r_{eq}} (r - r_{eq})^3 \\
 & + \frac{1}{4!} \left(\frac{d^4 V}{dr^4} \right)_{r_{eq}} (r - r_{eq})^4
 \end{aligned}$$

which should be looking vaguely familiar

$$V = \frac{1}{2} \sum_{ij} F_{ij} \Delta_i \Delta_j + \frac{1}{6} \sum_{ijk} F_{ijk} \Delta_i \Delta_j \Delta_k + \frac{1}{24} \sum_{ijkl} F_{ijkl} \Delta_i \Delta_j \Delta_k \Delta_l$$

Where did Taylor go?

Let's zoom in on the first term. Looking familiar?

Comparison

$$V(r)_{r_{eq}} \approx \frac{1}{2!} \left(\frac{d^2 V}{dr^2} \right)_{r_{eq}} (r - r_{eq})^2$$

$$V = \frac{1}{2} \sum_{ij} F_{ij} \Delta_i \Delta_j$$

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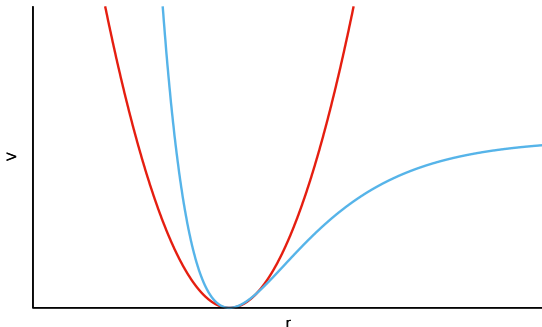
$$V = \frac{1}{2} \sum_{ij} F_{ij} \Delta_i \Delta_j$$

$$V = \frac{1}{2} kx^2$$

The first term is just the harmonic oscillator potential energy, accounting for the fact a second derivative can be two steps in one direction (like x^2), or one step in different directions (like $\Delta_i \Delta_j$)

What is a quartic force field?

Quartic just refers to the fourth-degree part of the Taylor series



The **quadratic** or **harmonic** terms give us the red curve, while the third- and fourth-order terms treat the **anharmonicity**, giving something like the blue curve.

How do we make one?

Let's go back to our full quartic equation

$$V = \frac{1}{2} \sum_{ij} F_{ij} \Delta_i \Delta_j + \frac{1}{6} \sum_{ijk} F_{ijk} \Delta_i \Delta_j \Delta_k + \frac{1}{24} \sum_{ijkl} F_{ijkl} \Delta_i \Delta_j \Delta_k \Delta_l$$

Of the terms here, we can “easily” get:

- ▶ $V \rightarrow$ comes out of Molpro
- ▶ $\Delta \rightarrow$ can be anything we want, typically 0.005 Å or radians

By the way, why the summations?

How do we make one?

To go from the scatterplot to a potential function, we have to

- ▶ Fit a function to our points, linear regression

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- ▶ Fit a function to our points, linear regression
- ▶ Use that function to calculate the force constants ($F_{i,j,k,l}$)

Recall

$$F = -\nabla V$$

How do we make one?

To go from the scatterplot to a potential function, we have to

- ▶ Fit a function to our points, linear regression
- ▶ Use that function to calculate the force constants ($F_{i,j,k,l}$)

Recall

$$F = -\nabla V$$

- ▶ Convert the force constants into frequencies

Harmonic oscillator again

$$\omega = \sqrt{\frac{k}{m}}$$

How do we make one?

“Fortunately” we have ancient programs that handle these steps for us

- ▶ Anpass - fits the function to our points and generates the force constants
- ▶ Spectro - determines the frequencies from the force constants
- ▶ Intder - the glue that holds all of the steps together

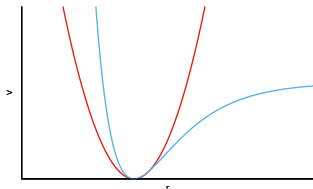


Getting started

Geometry optimization

Looking back at these, we see we need to start off at a good minimum

$$V(r)_{r_{eq}} \approx \frac{1}{0!} V(r_{eq}) + \frac{1}{1!} \left(\frac{dV}{dr} \right)_{r_{eq}} (r - r_{eq}) + \frac{1}{2!} \left(\frac{d^2V}{dr^2} \right)_{r_{eq}} (r - r_{eq})^2 + \frac{1}{3!} \left(\frac{d^3V}{dr^3} \right)_{r_{eq}} (r - r_{eq})^3 + \frac{1}{4!} \left(\frac{d^4V}{dr^4} \right)_{r_{eq}} (r - r_{eq})^4$$



Cancelling the second term, in particular, requires that we are at the minimum energy structure

Geometry optimization

Assuming Molpro

CCSD(T)-F12/cc-pVTZ-F12 example, also shortened to F12-TZ
(with my syntax highlighting “plugin”)

```
memory, 995, m;
gthresh,energy=1.d-12,zero=1.d-22,oneint=1.d-22,twoint=1.d-22;
gthresh,optgrad=1.d-8,optstep=1.d-8;
nocompress;
geometry={
0
H 1 oh
C 1 oc 2 hoc
N 3 cn 1 ocn 2 180.0
}

OH=          0.96399073  ANG
OC=          1.30253236  ANG
HOC=        109.54391210  DEG
CN=          1.16094343  ANG
OCN=        176.78899457  DEG

basis=cc-pVTZ-F12
{hf,maxit=500;wf,charge=0,spin=0;accu,20;}
{ccsd(t)-f12,maxit=250;wf,charge=0,spin=0;orbital,IGNORE_ERROR;}
{optg,grms=1.d-8,srms=1.d-8}
```

Project management (optimizing you)

What I do

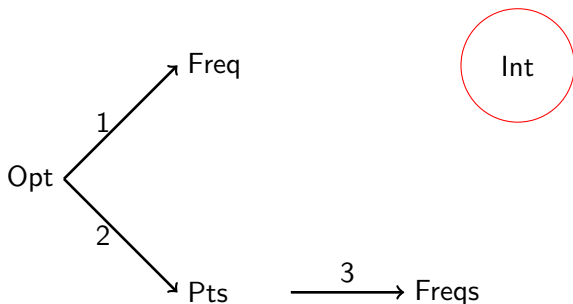
Once that's running, you have a little while to plan your attack

Molecule	Opt	Freq	Pts	Freqs	Int	Notes
H ₂ O	x	R	R		x	Warning in opt.out
H ₂ S	R				x	
S ₂ O	R				x	

- ▶ Opt - Molpro geometry optimization
- ▶ Freq - Molpro harmonic frequencies
- ▶ Pts - QFF single-point energies
- ▶ Freqs - QFF anharmonic frequencies
- ▶ Int - intensities, usually done in Gaussian

Project management

Dependencies/ordering



1 can be done with a script called `freqgen.sh`, and we'll cover the others now

Generating points

intder.in - anatomy

```
# INTDER #####
  4   6   6   0   0   3   0   0   0   1   0   0   0   1   1   0
STRE  1   2
STRE  2   3
STRE  3   4
BEND  2   3   4
LINX  4   3   2   1
LINY  4   3   2   1
  1   1  1.000000000
  2   2  1.000000000
  3   3  1.000000000
  4   4  1.000000000
  5   5  1.000000000
  6   6  1.000000000
  0

0.000000000  -0.010527465  2.462419282
0.000000000  -0.014386927   0.273628863
0.000000000   0.118270473  -2.179427573
0.000000000  -1.559616832  -2.884488088

DISP 743
  1  0.000000000
  0
  1 -0.020000000
  0
  1 -0.015000000
  2 -0.005000000
  0
```

Cartesian coordinates

0.000000000	-0.010527465	2.462419282
0.000000000	-0.014386927	0.273628863
0.000000000	0.118270473	-2.179427573
0.000000000	-1.559616832	-2.884488088

Generating points

intder.in - anatomy

```

# INTDER #####
 4   6   6   0   0   3   0   0   0   1   0   0   0   1   1   0
STRE 1   2
STRE 2   3
STRE 3   4
BEND 2   3   4
LINX 4   3   2   1
LINY 4   3   2   1
 1   1   1.000000000
 2   2   1.000000000
 3   3   1.000000000
 4   4   1.000000000
 5   5   1.000000000
 6   6   1.000000000
 0
      0.000000000      -0.010527465      2.462419282
      0.000000000      -0.014386927      0.273628863
      0.000000000      0.118270473      -2.179427573
      0.000000000      -1.559616832      -2.884488088
DISP 743
 1       0.000000000
 0
 1      -0.020000000
 0
 1      -0.015000000
 2      -0.005000000
 0

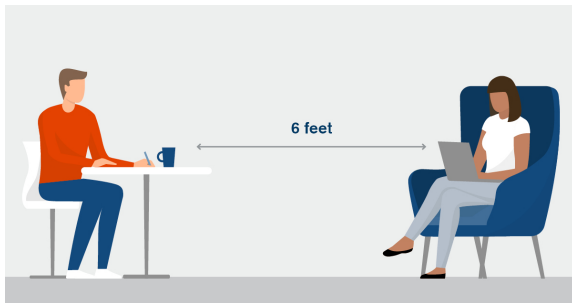
```

Displacements

Generating points

intder.in - general tips

- ▶ Spacing matters! Everywhere
- ▶ Don't use tabs
- ▶ Don't have trailing whitespace
- ▶ Copy a similar line from a known file to compare
- ▶ Spacing matters



Generating points

intder.in - general tips

That looks confusing. What do I actually change?

- ▶ Only the Cartesians for now (I think)
- ▶ Directives are in the manual if you really need them
- ▶ Internal coordinates are our next topic

Internal coordinates

Definition

Coordinates with an internal reference, in contrast to Cartesian coordinates, for example, which reference an external set of axes

```

0
H 1 OH
H 1 OH 2 HOH

OH = 1.0
HOH = 104.5
  
```

Figure: Z-matrix: (hopefully) familiar internal coordinates

```

3
water
0  0.000000  0.000000  0.000000
H  0.000000  0.000000  1.000000
H  0.968148  0.000000  -0.250380
  
```

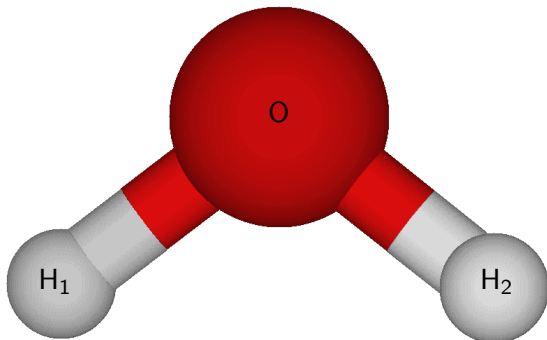
Figure: Cartesian coordinates

Internal coordinates

Simple internals

Definition

A single internal coordinate, like a bond stretch, bend, or torsion

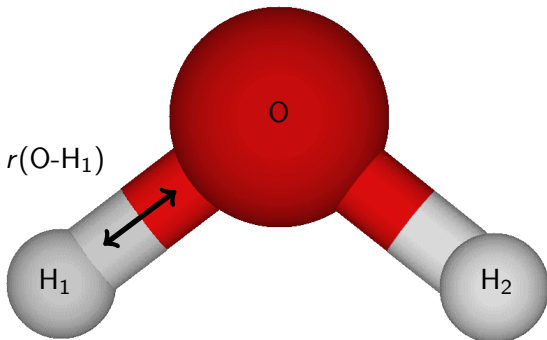


Internal coordinates

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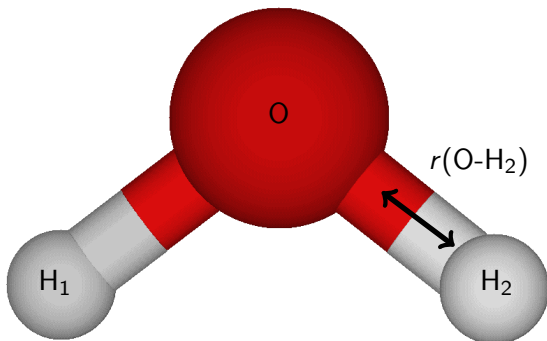


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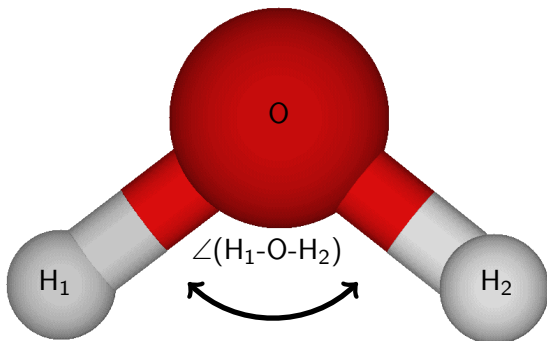


Internal coordinates

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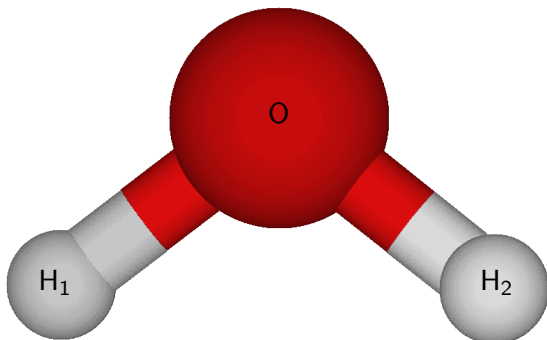


Internal coordinates

Symmetry internals

Definition

Linear combinations of simple internal coordinates



Internal coordinates

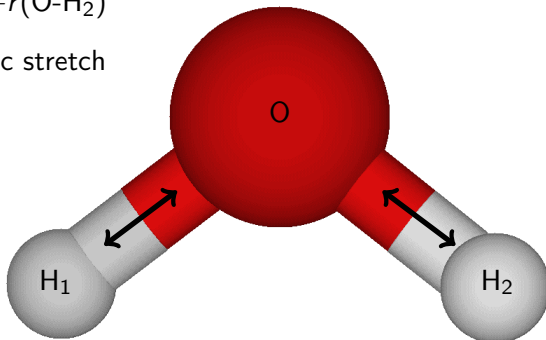
Symmetry internals

Definition

Linear combinations of simple internal coordinates

$$r(\text{O-H}_1) + r(\text{O-H}_2)$$

Symmetric stretch



Internal coordinates

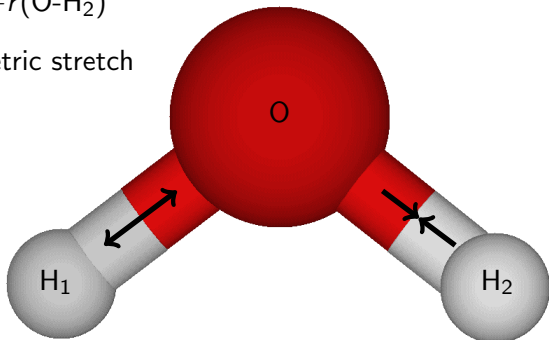
Symmetry internals

Definition

Linear combinations of simple internal coordinates

$$r(\text{O-H}_1) - r(\text{O-H}_2)$$

Anti-symmetric stretch

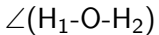


Internal coordinates

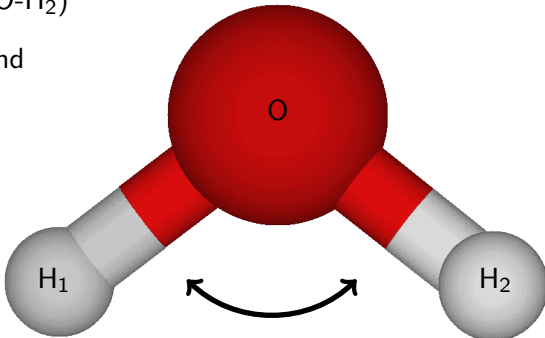
Symmetry internals

Definition

Linear combinations of simple internal coordinates



Bend



Symmetry

We can characterize a molecule, and its vibrational modes, based on symmetry. Water has C_{2v} symmetry, which is a pretty common one in our research.

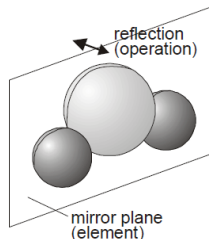
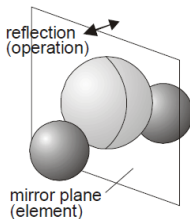
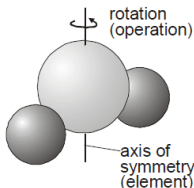
C_{2v}	E	$C_2(z)$	$\sigma_v(xz)$	$\sigma_v(yz)$	linear functions, rotations	quadratic functions	cubic functions
A_1	+1	+1	+1	+1	z	x^2, y^2, z^2	z^3, x^2z, y^2z
A_2	+1	+1	-1	-1	R_z	xy	xyz
B_1	+1	-1	+1	-1	x, R_y	xz	xz^2, x^3, xy^2
B_2	+1	-1	-1	+1	y, R_x	yz	yz^2, y^3, x^2y

Figure: Symmetry or character information is found in character tables

Symmetry

Symmetry operations

- ▶ Identity - E
- ▶ Rotation - C_n , at left
- ▶ Reflection - σ , at right
- ▶ Inversion - i , not shown
- ▶ Improper rotation - S_n , not shown
 - ▶ $S_1 = \sigma$
 - ▶ $S_2 = i$



Symmetry

- ▶ Usually rotations and reflections are enough to assign a symmetry, or when the symmetry is C_{2v} , that's all there is anyway.
- ▶ How do we do it?

Symmetry

- Usually rotations and reflections are enough to assign a symmetry, or when the symmetry is C_{2v} , that's all there is anyway.
- How do we do it? Back to the character table

C_{2v}	E	$C_2(z)$	$\sigma_v(xz)$	$\sigma_v(yz)$	linear functions, rotations	quadratic functions	cubic functions
A_1	+1	+1	+1	+1	z	x^2, y^2, z^2	z^3, x^2z, y^2z
A_2	+1	+1	-1	-1	R_z	xy	xyz
B_1	+1	-1	+1	-1	x, R_y	xz	xz^2, x^3, xy^2
B_2	+1	-1	-1	+1	y, R_x	yz	yz^2, y^3, x^2y

Symmetry

Determining symmetry

- ▶ Perform a symmetry operation
 - ▶ If the molecule looks the same, assign a 1
 - ▶ If the molecule looks the “opposite”, assign a -1
- ▶ Match your ± 1 values to rows of the character table

C_{2v}	E	$C_2(z)$	$\sigma_v(xz)$	$\sigma_v(yz)$	linear functions, rotations	quadratic functions	cubic functions
A_1	+1	+1	+1	+1	z	x^2, y^2, z^2	z^3, x^2z, y^2z
A_2	+1	+1	-1	-1	R_z	xy	xyz
B_1	+1	-1	+1	-1	x, R_y	xz	xz^2, x^3, xy^2
B_2	+1	-1	-1	+1	y, R_x	yz	yz^2, y^3, x^2y

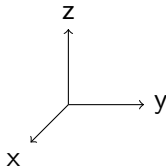
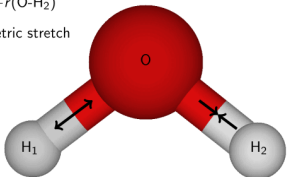
Symmetry

Determining symmetry

What is the symmetry of the anti-symmetric stretch in water? Let the main axis of rotation be the z-axis

C_{2v}	E	C ₂ (z)	σ _v (xz)	σ _v (yz)	linear functions, rotations	quadratic functions	cubic functions
A ₁	+1	+1	+1	+1	z	x ² , y ² , z ²	z ³ , x ² z, y ² z
A ₂	+1	+1	-1	-1	R _z	xy	xyz
B ₁	+1	-1	+1	-1	x, R _y	xz	xz ² , x ³ , xy ²
B ₂	+1	-1	-1	+1	y, R _x	yz	yz ² , y ³ , x ² y

$r(\text{O-H}_1) - r(\text{O-H}_2)$
 Anti-symmetric stretch



Symmetry

Why do we need it?

- ▶ Limits the number of displacements we have to calculate
- ▶ Part of what determines the IR activity of a mode
- ▶ It goes in your computational details

Generating points

intder.in - water

```
# INTDER #####
 4   6   6   0   0   3   0   0   0   1   0   0   0   1   1   0
STRE 1   2
STRE 2   3
STRE 3   4
BEND 2   3   4
LINX 4   3   2   1
LINY 4   3   2   1
 1   1   1.000000000
 2   2   1.000000000
 3   3   1.000000000
 4   4   1.000000000
 5   5   1.000000000
 6   6   1.000000000
 0
    0.000000000      -0.010527465      2.462419282
    0.000000000      -0.014386927      0.273628863
    0.000000000      0.118270473      -2.179427573
    0.000000000      -1.559616832      -2.884488088
DISP 743
 1      0.000000000
 0
 1      -0.020000000
 0
 1      -0.015000000
 2      -0.005000000
 0
```

Figure: Not water

Generating points

intder.in - water

```
# INTDER #####
3 3 3 0 0 3 0 0 0 1 0 0 0 1 1 0
STRE 1 2
STRE 1 3
BEND 2 1 3
1 1 1.000000000 2 1.000000000
2 1 1.000000000 2 -1.000000000
3 3 1.000000000
0
0.000000000 0.000000000 0.000000000
0.000000000 0.000000000 1.000000000
0.968140000 0.000000000 -0.250380000
```

Figure: Water

Generating points

Procedure

- ▶ Copy (yank) optimized geometry (in Bohr) from the Molpro log file
- ▶ Paste it into the `intder.in` file and make sure alignment is perfect
- ▶ Run `$ intder < intder.in > intder.out`
or something similar
- ▶ Use `pts-gen.py` to generate the single-point energy calculations from `intder` output
 - ▶ `$ pts-gen.py h2o O H H`
in our water example
- ▶ `$ cd inp && sh submit`
to submit the calculations

Gathering output

- ▶ Grab all the energies from output files
 - ▶ `$ grep "CCSD(T)-F12b" *.out > energy.dat`
or use `check.sh`
- ▶ Check that the number of energies is the same as the number of displacements
 - ▶ handy command for this is `$ wc -l filename`
"word count -lines"
 - ▶ `$ comp.py h2o`
to print missing ones to terminal
 - ▶ `$ comp.py h2o | sh`
to submit them right away
- ▶ Remember to rerun `grep` or `check.sh` after these run!

Preparing output

To minimize numerical noise, we want to work with relative energies. That is, we need to subtract the minimum energy from all of the other energies.

```
halsio3.0004.out: ICCSD(T)-F12b total energy -757.368358155773
halsio3.0005.out: ICCSD(T)-F12b total energy -757.368299271901
halsio3.0006.out: ICCSD(T)-F12b total energy -757.368349137881
halsio3.0007.out: ICCSD(T)-F12b total energy -757.368339420197
halsio3.0008.out: ICCSD(T)-F12b total energy -757.368365731733
halsio3.0009.out: ICCSD(T)-F12b total energy -757.368338574281
halsio3.0010.out: ICCSD(T)-F12b total energy -757.368241908086
halsio3.0011.out: ICCSD(T)-F12b total energy -757.368363416914
halsio3.0012.out: ICCSD(T)-F12b total energy -757.368280273263
halsio3.0013.out: ICCSD(T)-F12b total energy -757.368293617617
halsio3.0014.out: ICCSD(T)-F12b total energy -757.368370633874
halsio3.0015.out: ICCSD(T)-F12b total energy -757.368372577147
halsio3.0016.out: ICCSD(T)-F12b total energy -757.368368811868
```

```
0.000058595643
0.000117479515
0.000067613535
0.000077331219
0.000051019683
0.000078177135
0.000174843330
0.000053334502
0.000136478153
0.000123133799
0.000046117542
0.000044174269
0.000047939548
0.000044314622
0.000041851643
```

Figure: Want to go from this...

Figure: to this.

Use awk to do this, see relmaker.sh

Anpass

With the relative energies in hand, we are ready to fit them to a function

```

INPUT
TITLE
a12o2
INDEPENDENT VARIABLES
6
DATA POINTS
233 -2
(6F12.8, F20.12)
0.00000000 0.00000000 0.00000000 0.00000000 0.00000000 0.00000000 0.000000000000
-0.02000000 0.00000000 0.00000000 0.00000000 0.00000000 0.00000000 0.000175586858
-0.01500000 -0.00500000 0.00000000 0.00000000 0.00000000 0.00000000 0.0001600399569
-0.01500000 0.00000000 0.00000000 0.00000000 0.00000000 0.00000000 0.000090228397
-0.01500000 0.00500000 0.00000000 0.00000000 0.00000000 0.00000000 0.000106381061
-0.01000000 -0.01000000 0.00000000 0.00000000 0.00000000 0.00000000 0.000059936736
-0.01000000 -0.00500000 0.00000000 0.00000000 0.00000000 0.00000000 0.000046525039
-0.01000000 0.00000000 -0.01000000 0.00000000 0.00000000 0.00000000 0.000073355273
-0.01000000 0.00000000 0.00000000 -0.01000000 0.00000000 0.00000000 0.000048164266
-0.01000000 0.00000000 0.00000000 0.00000000 -0.01000000 0.00000000 0.000083096066
-0.01000000 0.00000000 0.00000000 0.00000000 0.00000000 -0.01000000 0.000077338116
-0.01000000 0.00000000 0.00000000 0.00000000 0.00000000 0.00000000 0.000043367402
-0.01000000 0.00000000 0.00000000 0.00000000 0.00000000 0.01000000 0.000077338121
-0.01000000 0.00000000 0.00000000 0.00000000 0.01000000 0.00000000 0.000083096107
-0.01000000 0.00000000 0.00000000 0.01000000 0.00000000 0.00000000 0.000048164264
-0.01000000 0.00000000 0.01000000 0.00000000 0.00000000 0.00000000 0.000073355222
-0.01000000 0.00500000 0.00000000 0.00000000 0.00000000 0.00000000 0.000050408282
-0.01000000 -0.01000000 0.00000000 0.00000000 0.00000000 0.00000000 0.000057912224
-0.00500000 -0.01500000 0.00000000 0.00000000 0.00000000 0.00000000 0.000053731551
-0.00500000 -0.01000000 0.00000000 0.00000000 0.00000000 0.00000000 0.000029200483
-0.00500000 -0.00500000 -0.01000000 0.00000000 0.00000000 0.00000000 0.000044259147
-0.00500000 -0.00500000 0.00000000 -0.01000000 0.00000000 0.00000000 0.000019722496
-0.00500000 -0.00500000 0.00000000 0.00000000 -0.01000000 0.00000000 0.000054146554
-0.00500000 -0.00500000 0.00000000 0.00000000 0.00000000 -0.01000000 0.000048330219
-0.00500000 -0.00500000 0.00000000 0.00000000 0.00000000 0.00000000 0.000014855027
-0.00500000 -0.00500000 0.00000000 0.00000000 0.00000000 0.01000000 0.000048330227
-0.00500000 -0.00500000 0.00000000 0.00000000 0.01000000 0.00000000 0.000054146555
-0.00500000 -0.00500000 0.00000000 0.01000000 0.00000000 0.00000000 0.000019722511
-0.00500000 -0.00500000 0.01000000 0.00000000 0.00000000 0.00000000 0.000044259223

```

Figure: Example anpass input file

Anpass

Formatting is again very important!

```
INPUT
TITLE
a1262
INDEPENDENT VARIABLES
    0
DATA POINTS
233 -2
(8F12.8, F20.12)
 0.00000000 0.00000000 0.00000000 0.00000000 0.00000000 0.00000000 0.000000000000
-0.02000000 0.00000000 0.00000000 0.00000000 0.00000000 0.00000000 0.00017586858
-0.01500000 -0.00500000 0.00000000 0.00000000 0.00000000 0.00000000 0.000100399569
-0.01500000 0.00000000 0.00000000 0.00000000 0.00000000 0.00000000 0.00009828397
-0.01500000 0.00500000 0.00000000 0.00000000 0.00000000 0.00000000 0.000106381061
-0.01000000 -0.01000000 0.00000000 0.00000000 0.00000000 0.00000000 0.000059936736
-0.01000000 -0.00500000 0.00000000 0.00000000 0.00000000 0.00000000 0.000046525039
-0.01000000 0.00000000 -0.01000000 0.00000000 0.00000000 0.00000000 0.000073355273
-0.01000000 0.00000000 0.00000000 -0.01000000 0.00000000 0.00000000 0.000048164206
-0.01000000 0.00000000 0.00000000 0.00000000 -0.01000000 0.00000000 0.000083090606
-0.01000000 0.00000000 0.00000000 0.00000000 0.00000000 -0.01000000 0.000077338116
-0.01000000 0.00000000 0.00000000 0.00000000 0.00000000 0.00000000 0.000043367402
-0.01000000 0.00000000 0.00000000 0.00000000 0.00000000 0.01000000 0.000077338121
-0.01000000 0.00000000 0.00000000 0.00000000 0.01000000 0.00000000 0.000083096167
-0.01000000 0.00000000 0.00000000 0.01000000 0.00000000 0.00000000 0.000048164204
-0.01000000 0.00000000 0.01000000 0.00000000 0.00000000 0.00000000 0.000073355222
-0.01000000 0.00500000 0.00000000 0.00000000 0.00000000 0.00000000 0.000050488282
-0.01000000 0.01000000 0.00000000 0.00000000 0.00000000 0.00000000 0.000067912224
-0.00500000 -0.01500000 0.00000000 0.00000000 0.00000000 0.00000000 0.000053731551
-0.00500000 -0.01000000 0.00000000 0.00000000 0.00000000 0.00000000 0.000029200483
-0.00500000 -0.00500000 -0.01000000 0.00000000 0.00000000 0.00000000 0.000044259147
-0.00500000 -0.00500000 0.00000000 -0.01000000 0.00000000 0.00000000 0.000019722496
-0.00500000 -0.00500000 0.00000000 0.00000000 -0.01000000 0.00000000 0.000054146554
-0.00500000 -0.00500000 0.00000000 0.00000000 0.00000000 -0.01000000 0.000048330219
-0.00500000 -0.00500000 0.00000000 0.00000000 0.00000000 0.00000000 0.000014855027
-0.00500000 -0.00500000 0.00000000 0.00000000 0.00000000 0.01000000 0.000048330227
-0.00500000 -0.00500000 0.00000000 0.00000000 0.01000000 0.00000000 0.000054146555
-0.00500000 -0.00500000 0.00000000 0.01000000 0.00000000 0.00000000 0.000019722511
-0.00500000 0.00500000 0.01000000 0.00000000 0.00000000 0.00000000 0.000044259223
```

Figure: Example anspass input file

Anpass

Once the input file is set up:

- ▶ Run `anpass` with `$ anpass < anpass1.in > anpass1.out`
 - ▶ Notice the 1 here, this is the first of two `Anpass` runs
- ▶ Go to the bottom of the first output file and make sure the sum of squared residuals is less than about 10^{-16}

```

230     0.000104625002     0.000104625125     -1.22040445E-10
231     0.000096649148     0.000096649207     -5.86328577E-11
232     0.000098727188     0.000098727289     -1.80916664E-10
233     0.000170898999     0.000170898946     -3.73331127E-11
ONEIGHTED SUM OF SQUARED RESIDUALS IS    1.24638046E-18

        M I N I M U M
WHERE ENERGY IS          -0.00000000547
   AT      -0.0000351027
            0.000051470
            0.000000000
            0.000000000
            0.000000000
            0.000000000
            0.000000000
            -0.000035102685      0.00005147046      0.000000000000      0.000000000000      0.000000000000
000000 -0.00000000547
BEIGENVALUE(S) OF HESSIAN, STARTING WITH LOWEST
BEIGENVALUE    1      0.99123759E+01      0.00000000      0.00000000      0.00000000
                0.00000000      0.00000000
BEIGENVALUE    2      0.40413757E+00
                -0.08539873      -0.59634686      0.00000000      0.00000000
                0.00000000      0.00000000
BEIGENVALUE    3      0.37678322E+00
                0.00000000      0.00000000      1.00000000      0.00000000
                0.00000000      0.00000000
BEIGENVALUE    4      0.66049638E+00
                0.00000000      0.00000000      0.00000000      0.00000000
                0.00000000      1.00000000
BEIGENVALUE    5      0.77581686E+00
                0.00000000      0.00000000      0.00000000      0.00000000
                1.00000000      0.00000000
BEIGENVALUE    6      0.00950155E+00
  
```

Anpass

After this:

- ▶ Copy anpass1.in to anpass2.in
- ▶ Copy the “long line” from anpass1.out to the bottom of anpass1.in, above END OF DATA
- ▶ Cut the !STATIONARY POINT line and paste it above the “long line”

```
230 0.000104623002 0.000104625125 -1.22649445E-10
231 0.000096649148 0.000096649207 -5.86328577E-11
232 0.000098727188 0.000098727289 -1.00916064E-10
233 0.000170898909 0.000170898946 -3.73331127E-11
WEIGHTED SUM OF SQUARED RESIDUALS IS 1.24030046E-10

0 M I N I M U M

WHERE ENERGY IS -0.000000000547
AT -0.0000351027
0.0000051470
0.0000000000
0.0000000000
0.0000000000
0.0000000000
0.0000000000
-0.000035102685 0.000005147046 0.000000000000 0.000000000000 0.000000000000 0.000000000000
00000 -0.000000000547
EIGENVALUE(S) OF HESSIAN, STARTING WITH LOWEST
EIGENVALUE 1 0.59122759E+01
0.00000000 0.00000000 0.00000000 1.00000000
0.00000000 0.00000000
EIGENVALUE 2 0.48413757E+00
-0.00539873 -0.99634696 0.00000000 0.00000000
0.00000000 0.00000000
EIGENVALUE 3 0.57672832E+00
0.00000000 0.00000000 1.00000000 0.00000000
0.00000000 0.00000000
EIGENVALUE 4 0.66049638E+00
0.00000000 0.00000000 0.00000000 0.00000000
0.00000000 1.00000000
EIGENVALUE 5 0.77581686E+00
0.00000000 0.00000000 0.00000000 0.00000000
1.00000000 0.00000000
```

Anpass

```

0.01500000  0.00500000  0.00000000  0.00000000  0.00000000  0.00000000  0.00000000  0.000104625125
0.01500000  0.00000000  0.00000000  0.00000000  0.00000000  0.00000000  0.00000000  0.000096649207
0.01500000  0.00500000  0.00000000  0.00000000  0.00000000  0.00000000  0.00000000  0.000098727289
0.02000000  0.00000000  0.00000000  0.00000000  0.00000000  0.00000000  0.00000000  0.000170890946
UNKNOWN
53
FUNCTION
0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0
0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  1  1  1
1  1  1  1  1  1  1  1  1  1  1  2  2  2  2  2  2
2  2  3  3  4
0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0
0  1  1  1  1  1  1  2  2  2  2  2  3  4  0  0  0
0  0  0  0  1  1  1  1  1  2  3  0  0  0  0  0  0
1  2  0  1  0
0  0  0  0  0  0  0  0  0  0  1  2  2  2  2  2
4  0  0  0  0  1  2  0  0  0  0  2  0  0  0  0
0  0  1  2  0  0  0  0  2  0  0  0  0  0  0  2
0  0  0  0
0  0  0  0  0  0  2  2  2  4  0  1  0  0  0  2
0  0  0  0  2  0  0  0  0  0  2  0  0  0  0  0
0  2  0  0  0  0  0  2  0  0  0  0  0  0  2  0
0  0  0  0
0  0  0  2  2  4  0  0  2  0  1  1  0  0  2  0
0  0  0  2  0  1  0  0  0  2  0  0  0  0  0  0
2  0  1  0  0  0  2  0  0  0  0  0  0  2  0  0
0  0  0  0  0
0  2  4  0  0  2  0  0  2  0  0  1  1  0  2  0  0
0  0  2  0  0  1  0  0  2  0  0  0  0  0  0  2
0  0  1  0  0  2  0  0  0  0  0  0  2  0  0  0
0  0  0  0
END OF DATA
!FIT
!STATIONARY POINT
!END

```

Figure: anpass1.in bottom

Anpass

```
0.01500000 0.00500000 0.00000000 0.00000000 0.00000000 0.00000000 0.000104025125
0.01500000 0.00000000 0.00000000 0.00000000 0.00000000 0.00000000 0.000096649207
0.01500000 0.00500000 0.00000000 0.00000000 0.00000000 0.00000000 0.000098727289
0.02000000 0.00000000 0.00000000 0.00000000 0.00000000 0.00000000 0.000170890946
UNKNOWN5
53
FUNCTION
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
0 0 0 0 0 0 0 0 0 0 0 0 0 0 1 1
1 1 1 1 1 1 1 1 1 1 1 2 2 2 2 2
2 2 3 3 4
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
0 1 1 1 1 1 2 2 2 2 2 3 4 0 0 0
0 0 0 0 1 1 1 1 1 2 3 0 0 0 0 0
1 2 0 1 0
0 0 0 0 0 0 0 0 0 0 1 1 2 2 2 2
4 0 0 0 0 1 2 0 0 0 0 2 0 0 0 0
0 0 1 2 0 0 0 0 2 0 0 0 0 0 0 2
0 0 0 0 0
0 0 0 0 0 0 2 2 2 4 0 1 0 0 0 2
0 0 0 0 2 0 0 0 0 0 2 0 0 0 0 0
0 2 0 0 0 0 0 2 0 0 0 0 0 0 2 0
0 0 0 0 0
0 0 0 2 2 4 0 0 2 0 1 1 0 0 2 0
0 0 0 2 0 1 0 0 0 2 0 0 0 0 0 0
2 0 1 0 0 0 2 0 0 0 0 0 0 2 0 0
0 0 0 0 0
0 2 4 0 2 0 0 2 0 0 1 1 0 2 0 0
0 0 2 0 0 1 0 0 2 0 0 0 0 0 0 2
0 0 1 0 0 2 0 0 0 0 0 0 2 0 0 0
0 0 0 0 0
STATIONARY POINT
-0.000035102685 0.000005147046 0.000000000000 0.000000000000 0.000000000000 0.000000000000
00000 -0.000000000547
END OF DATA
IFIT
END
273.1 Bot
```

Figure: anpass2.in bottom

Anpass

What is the long line?

- ▶ In fitting our function, anpass can find a new minimum that is slightly different from the one from Molpro
- ▶ The long line is the series of displacements that correspond to this minimum, along with its energy
- ▶ The “!” is a comment, so we are telling anpass that the long line is a stationary point and to run a slightly different calculation

Anpass

The other important thing `anpass` gives us are the force constants in `fort.9903`

```

53
 0  0  0  0  0.000000000288
 6  6  0  0  2.879641150306
 6  6  6  6  3.268664626615
 5  5  0  0  3.382416943673
 6  6  5  5 16.919503402043
 5  5  5  5  7.720549618100
 4  4  0  0  0.432161118353
 6  6  4  4 -3.489227624058
 5  5  4  4 -4.247795562121
 4  4  4  4  2.317438189761
 6  5  3  0 -9.100591142294
 6  5  4  3 -0.014823366425
 3  3  0  0  2.514428022426
 6  6  3  3 22.039113667990
 5  5  3  3 21.784976166893

```

Figure: `fort.9903`

This takes us back into `intder`

Intder

`intder_geom.in`

Anpass gave us a new equilibrium geometry in terms of symmetry internal coordinate displacements. We need to use Intder to turn that into a Cartesian geometry. Intder's main purpose is undertaking these transformations for us, hence calling it the glue

- ▶ Copy your `intder.in` file from `pts` and call it `intder_geom.in`
- ▶ Change the number of displacements to 1 and delete all of the displacements
 - ▶ You may want to keep at least one or two for alignment reference
- ▶ Take the nonzero lines from under WHERE ENERGY IS AT in `anpass1.out` to be the new displacements

Intder

intder_geom.in

I'm mixing my examples here unfortunately, so pay attention to the displacements section only

```
intder.in
4 6 6 0 0 3 0 0 0 1 0 0 0 1 1 0
STRE 1 2
STRE 2 3
STRE 3 4
BEND 2 3 4
LINX 4 3 2 1
LINY 4 3 2 1
1 1 1.000000000
2 2 1.000000000
3 3 1.000000000
4 4 1.000000000
5 5 1.000000000
6 6 1.000000000
0
0.000000000 -0.010527465 2.462419282
0.000000000 -0.014306927 0.273628863
0.000000000 0.118270473 -2.179427573
0.000000000 -1.559616832 -2.884488088
DISP 743
1 0.000000000
0
1 -0.020000000
0
1 -0.015000000
2 -0.005000000
0
```

Figure: intder.in from pts

```
intder_geom.in
4 7 6 0 0 3 0 0 0 1 0 0 0 1 1 0
STRE 1 2
STRE 1 3
STRE 2 4
STRE 3 4
STRE 1 4
STRE 2 3
TORS 4 3 2 1
1 5 1.000000000 6 1.000000000
2 5 1.000000000 6 -1.000000000
3 1 1.000000000 2 -1.000000000 3 -1.000000000 4 1.000000000
4 7 1.000000000
5 1 1.000000000 2 1.000000000 3 -1.000000000 4 -1.000000000
6 1 1.000000000 2 -1.000000000 3 1.000000000 4 -1.000000000
0
0.000000000 2.391678166 0.000000000
-2.274263181 0.000000000 0.000000000
2.274263181 0.000000000 0.000000000
0.000000000 -2.391678166 0.000000000
DISP 1
1 -0.0000351027
2 0.0000051470
0
```

Figure: intder_geom.in

These are the same numbers from the long line, but formatted more easily for our use

Intder

intder.in

intder_geom will produce a new equilibrium geometry in Cartesian coordinates that we can stick back in to a slightly different type of intder file

- ▶ Copy any intder.in to the freqs directory
- ▶ Take the new geometry from the very bottom of intder_geom.out and replace the one in intder.in
- ▶ Delete everything below the Cartesian coordinates
- ▶ The next line needs to be the atoms, with their masses
 - ▶ You almost definitely want to copy one of these lines from another file to get the alignment right

Intder

intder.in

```
# INTDER #####  
4 7 6 4 0 3 2 0 0 1 3 0 0 0 0  
STRE 1 2  
STRE 1 3  
STRE 2 4  
STRE 3 4  
STRE 1 4  
STRE 2 3  
TORS 4 3 2 1  
1 5 1.000000000 6 1.000000000  
2 5 1.000000000 6 -1.000000000  
3 1 1.000000000 2 -1.000000000 3 -1.000000000 4 1.000000000  
4 7 1.000000000  
5 1 1.000000000 2 1.000000000 3 -1.000000000 4 -1.000000000  
6 1 1.000000000 2 -1.000000000 3 1.000000000 4 -1.000000000  
0  
0.000000000 2.391678166 0.000000000  
-2.274263181 0.000000000 0.000000000  
2.274263181 0.000000000 0.000000000  
0.000000000 -2.391678166 0.000000000  
016 AL27 AL27 016
```

Figure: Our intder.in file so far

Intder

intder.in

Now we need to read in the force constants from fort.9903

- ▶ You can read fort.9903 in directly with `:r fort.9903`, but there is a lot of processing to do
- ▶ Instead, use `format.sh`; there are two ways to use it:
 - ▶ My preferred way is to run it from inside vim with `:r !format.sh`
 - ▶ But you can also run it at the command line `$ format.sh > intder.bot`
and save the output into a file that you then read in to `intder.in`

Intder

intder.in

```
# INTDER #####
 4 7 6 4 0 3 2 0 0 1 3 0 0 0 0 0
STRE 1 2
STRE 1 3
STRE 2 4
STRE 3 4
STRE 1 4
STRE 2 3
TORS 4 3 2 1
 1 5 1.00000000 6 1.00000000
 2 5 1.00000000 6 -1.00000000
 3 1 1.00000000 2 -1.00000000 3 -1.00000000 4 1.00000000
 4 7 1.00000000
 5 1 1.00000000 2 1.00000000 3 -1.00000000 4 -1.00000000
 6 1 1.00000000 2 -1.00000000 3 1.00000000 4 -1.00000000
 0
 0.00000000 2.391678166 0.00000000
-2.274263181 0.00000000 0.00000000
 2.274263181 0.00000000 0.00000000
 0.00000000 -2.391678166 0.00000000
 016 AL27 AL27 016
 6 6 0 0 2.879641150306
 5 5 0 0 3.382416943673
 4 4 0 0 0.432161118353
 3 3 0 0 2.514428022426
 2 2 0 0 1.776761156544
 2 1 0 0 -0.172632546873
 1 1 0 0 3.776068088560
 0
 6 6 2 0 0.318910045240
 5 5 2 0 -0.626237143238
 4 4 2 0 0.174503785575
 6 5 3 0 -9.100591142294
```

Figure: Part of the final intder.in file

Intder

intder.out

- ▶ Run intder: `$ intder < intder.in > intder.out`
- ▶ Verify that the harmonic frequencies at the very bottom correspond to those from Molpro (if those have finished)
- ▶ Run `$ tennis.sh` to move the intder output files to the filenames expected by spectro

```

ZERO FREQUENCIES (OH-1)
-0.0078 -0.0069 -0.0000 0.0000 0.0000 0.0078

VIBRATIONAL FREQUENCIES (OH-1) AND EIGENVECTORS
-----
COORDINATE 1 2 3 4 5 6
1 -0.000000 0.000000 0.177409 -0.140092 -0.000000 0.000000
2 -0.000000 0.000000 0.000000 0.000000 0.140092 -0.122392
3 -0.140092 0.000000 0.000000 0.000000 -0.000000 0.000000
4 -0.000000 0.117332 0.000000 0.003040 -0.000000 0.000000
5 -0.000000 0.000000 -0.002663 0.000000 -0.003040 -0.000000
6 0.003040 -0.000000 -0.000000 0.000000 0.000000 0.000000
7 0.000000 -0.117332 0.000000 0.003040 0.000000 -0.000000
8 0.000000 0.000000 0.002663 0.000000 -0.003040 0.000000
9 0.003040 0.000000 0.000000 0.000000 0.000000 0.000000
10 -0.000000 0.000000 -0.177409 -0.140092 0.000000 0.000000
11 0.000000 -0.002663 0.000000 0.000000 0.140092 0.152391
12 -0.140092 0.000000 0.000000 0.000000 0.000000 0.000000
-----

MODE OH-1
1 302.0
2 324.3
3 847.7
4 679.9
5 774.9
6 895.4

```

Spectro

spectro.in

You should be given a spectro.in file looking something like this

```

# SPECTRO #####
  1  1  3  2  0  0  1  4  0  0  0  0  0  0
  1  1  0  0  0  1  0  0  0  0  0  0  0  0
# GEOM #####
  4  1
  8.00  0.00000000  2.391678166  0.000000000
 13.00 -2.274263181  0.000000000  0.000000000
 13.00  2.274263181  0.000000000  0.000000000
  8.00  0.000000000 -2.391678166  0.000000000
# WEIGHT #####
  4
  1  15.994915
  2  26.981539
  3  26.981539
  4  15.994915
# CURVIL #####
  1  2
  1  3
  1  4
  1  4  2
  1  4  3
  4  3  2  1
# FERMI1 #####
  1
  6  5
# CORIOL #####
  3
  0
  3  2  0  0  1
  0
  4  1  0  0  1
  0
  5  4  0  0  1

```

Spectro

spectro.in

Don't worry about these, probably

Input directives, see manual

```

# SPECTRO #####
 1  1  3  2  0  0  1  4  0  0  0  0  0  0
 1  1  0  0  0  1  0  0  0  0  0  0  0  0
# GEOM #####
4  1
8.00  0.00000000  2.391678166  0.000000000
13.00 -2.274263181  0.000000000  0.000000000
13.00  2.274263181  0.000000000  0.000000000
8.00  0.000000000  -2.391678166  0.000000000
# WEIGHT #####
4
1  15.994915
2  26.981539
3  26.981539
4  15.994915
# CURVIL #####
1  2
1  3
1  4
1  4  2
1  4  3
4  3  2  1
# FERMI1 #####
1
6  5
# CORIOL #####
3
0
3  2  0  0  1
0
4  1  0  0  1

```

Spectro

spectro.in

You will definitely need to change these

```
# SPECTRO #####
1 1 3 2 0 0 1 4 0 0 00 0 0 0 0
1 1 0 0 0 1 0 0 0 0 0 0 0 0 0
# GEOM #####
4 1
8.00 0.00000000 2.391678166 0.00000000
13.00 -2.274263181 0.00000000 0.00000000
13.00 2.274263181 0.00000000 0.00000000
8.00 0.00000000 -2.391678166 0.00000000
# WEIGHT #####
4
1 15.994915
2 26.981539
3 26.981539
4 15.994915
# CURVIL #####
1 2
1 3
1 4
1 4 2
1 4 3
4 3 2 1
# FERMI1 #####
1
6 5
# CORIOL #####
3
0
3 2 0 0 1
0
4 1 0 0 1
0
5 4 0 0 1
```

Geometry

Spectro

spectro.in

Change these too, from nist.gov/pml/atomic-weights-and-isotopic-compositions-relative-atomic-masses

```
# SPECTRO #####
1 1 3 2 0 0 1 4 0 0 00 0 0 0 0
1 1 0 0 0 1 0 0 0 0 0 0 0 0 0
# GEOM #####
4 1
8.00 0.00000000 2.391678166 0.00000000
13.00 -2.274263181 0.000000000 0.000000000
13.00 2.274263181 0.000000000 0.000000000
8.00 0.000000000 -2.391678166 0.000000000
# WEIGHT #####
4
1 15.994915
2 26.981539
3 26.981539
4 15.994915
# CORIOL #####
1 2
1 3
1 4
1 4 2
1 4 3
4 3 2 1
# FERMI1 #####
1
6 5
# CORIOL #####
3
0
3 2 0 0 1
0
```

Masses

Spectro

spectro.in

You shouldn't need to touch these, they should resemble the simple internals from intder

```

# SPECTRO *****
1 1 3 2 0 0 1 4 0 0 0 0 0 0
1 1 0 0 0 1 0 0 0 0 0 0 0 0 0
# GEOM *****
4 1
8.00 0.00000000 2.391678166 0.00000000
13.00 -2.274263181 0.00000000 0.00000000
13.00 2.274263181 0.00000000 0.00000000
8.00 0.00000000 -2.391678166 0.00000000
# WEIGHT *****
4
1 15.994915
2 26.981539
3 26.981539
4 15.994915
# CURVIL *****
1 2
1 3
1 4
1 4 2
1 4 3
4 3 2 1
# TORSION *****
1
6 5
# CORIOL *****
3
0
3 2 0 0 1
0
4 1 0 0 1
0
5 4 0 0 1

```

Curvilinear coordinates

Spectro

spectro.in

We'll talk more about these in a minute

```

# SPECTRO #####
 1  1  3  2  0  0  1  4  0  0  00  0  0  0  0
 1  1  0  0  0  0  1  0  0  0  0  0  0  0  0
# GEOM #####
 4  1
8.00  0.00000000  2.391678166  0.00000000
13.00 -2.274263181  0.000000000  0.00000000
13.00  2.274263181  0.000000000  0.00000000
 8.00  0.000000000  -2.391678166  0.00000000
# WEIGHT #####
 4
 1  15.994915
 2  26.981539
 3  26.981539
 4  15.994915
# CURVIL #####
 1  2
 1  3
 1  4
 1  4  2
 1  4  3
 1  3  2
# FERMI1 #####
 1
 6  5
# CORIOL #####
 3
 0
 3  2  0  0  1
 0
 4  1  0  0  1
 0
 5  4  0  0  1

```

Resonances

Spectro

spectro.out

- ▶ Run spectro with
\$ spectro < spectro.in > spectro.out
- ▶ Open spectro.out and search for “FUND” and it should look something like below

```

6          0.260      -0.739      -0.896      -2.181      0.368      0.018
*****
BAND CENTER ANALYSIS
*****
MODE      HARMONIC      FUNDAMENTAL      DIFFERENCE
1         805.408      794.559          10.849
2         774.882      762.614          12.268
3         679.875      667.160          12.714
4         647.702      634.930          12.772
5         524.333      520.772           3.561
6         301.995      300.408           1.587
E0 IS THE DUNHAM COEF
ONLY RELEVANT IN THERMODYNAMICS
*****
KKKK SUMMED COMPONENT IS      1.15924723174358
KKK  SUMMED COMPONENT IS     -0.286741453159454
KKL  SUMMED COMPONENT IS      1.34137762821829
KLM  SUMMED COMPONENT IS      3.22879653963718
E_o IS      5.44267994643959
*****
*****

```


Spectro

spectro.out

- ▶ Now, jump to the top and search for “FERMI”
 - ▶ This will take you to the resonances
 - ▶ We only worry about the Fermi and Coriolis ones

```

*****
CORIOLIS RESONANCES                WI = WJ
*****
  I   J   WI      WJ      DIFF      ZETA  DeltaALPHA
ALPHA 3C  2   679.87  774.88  -95.01  -1.000  -0.00458
ALPHA 4C  1   647.70  805.41  -157.71 -0.351  -0.00034
ALPHA 5C  4   524.33  647.70  -123.37 -0.936  -0.00311
*****

FERMI RESONANCE                TYPE 1                2WI = WJ
*****
  I   I   J      WI      WJ      DIFF      PHI IJ  EST.PERTURB.
X   6   6   5   301.99  524.33  79.66      -11.380      0.000
*****

FERMI RESONANCE                TYPE 2                WA = WB + WC
*****
  I   J   K      WI      WJ      WK      PHI IJK  WJ+WK-WI  EST.PERTURB.
THIS TYPE OF FERMI RESONANCE NOT FOUND
*****

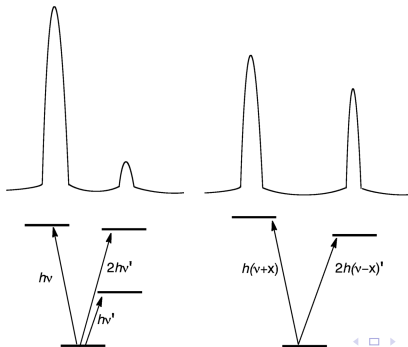
DARLING-DENNISON RESONANCES                2WI = 2WJ
*****
  I   J      WI      WJ      DIFF
2     1   774.88  805.41  61.05

```

What is a resonance?

Fermi resonance

If two vibrational modes have the same symmetry and similar energies, the higher energy mode will shift to higher energy and the lower to lower energy, basically to get away from each other



What is a resonance?

The definition may be slightly different for Coriolis resonances, but there wasn't a Wikipedia page

Fermi type 1

An overtone band, an integer multiple of one frequency, has a frequency similar to that of another band.

We see an example of this in our spectro.out file. $2\nu_6 \approx \nu_5$

```

*****
      FERMI RESONANCE          TYPE 1          2WI = WJ
*****
      I  I  J      WI          WJ          DIFF          PHI IJ  EST.PERTURB.
X  6  6  5      301.99      524.33      79.66          -11.380      0.000

```

80 cm^{-1} is a pretty huge difference, so the estimated perturbation is zero, but often these frequencies line up perfectly and have a substantial effect

What is a resonance?

Fermi type 2

The combination of two lower frequency modes have a frequency similar to one higher frequency mode.

Example

Let $\nu_6 = 234.5$, $\nu_5 = 364.3$, and $\nu_2 = 600.1 \text{ cm}^{-1}$.

Then $\nu_6 + \nu_5 = 598.8 \approx \nu_2$, and we could expect a larger perturbation than seen for our type 1 example.

Spectro

spectro.in again

How do we account for these resonances? We already saw how to handle type I resonances in the example spectro file

```
# FERMI1 #####
      1
      6      5
```

This says that we have one type 1 Fermi resonance, in which $2\nu_6 = \nu_5$.

Spectro

spectro.in again

To handle a type 2 Fermi resonance, such as the one in our example, we would add another block like this:

```
# FERMI2 #####
1
6      5      2
```

which again says that $\nu_6 + \nu_5 = \nu_2$

Spectro

spectro.in again

Fermi polyad

We can also have a situation where multiple combinations come close to a single frequency. For example, both $\nu_6 + \nu_5$ and $2\nu_4$ could be close to ν_2 . This results in a Fermi polyad, which should be handled separately.

```
# FERMI1 #####
3
6 5
4 1
5 1
# RESIN #####
1
5
1 0 0 0 0 0
0 0 0 0 1 0
0 0 0 2 0 0
0 0 0 0 2 0
0 0 0 0 0 2
```

Figure: Handling a Fermi polyad for Ti_2O_2

Spectro

spectro.in again

Basically if you have a polyad you need to make one of those RESIN arrays. Everything on the right hand side of the equation gets a row with a one in its column, and everything on the left hand side gets a row. In the previous example, we had a row

$$1 \quad 0 \quad 0 \quad 0 \quad 0 \quad 0$$

which represents ν_1 , which appeared in two type 1 Fermi resonances, $2\nu_4 = \nu_1$ and $2\nu_5 = \nu_1$. The corresponding row for ν_5 is

$$0 \quad 0 \quad 0 \quad 0 \quad 1 \quad 0$$

Spectro

spectro.in again

The combinations of modes that make ν_5 and ν_1 get their own rows. Since in this case they are type 1 Fermi resonances, there are twos in those positions. For $2\nu_4$, which equals ν_1 , we get the row

$$0 \quad 0 \quad 0 \quad 2 \quad 0 \quad 0$$

and so on. If we had a type 2 Fermi resonance, say $\nu_3 + \nu_4 = \nu_1$ too, we would add a row that looks like

$$0 \quad 0 \quad 1 \quad 1 \quad 0 \quad 0$$

The ordering of these rows does not matter, just make sure that every left and right hand side is accounted for in equations like $\nu_3 + \nu_4 = \nu_1$.

Spectro

spectro.in again

Coriolis resonances

I'm not as sure about the physical meaning of these, but think of them the same way. Some combination of frequencies bumps into each other and wants to push the other away. Regardless, we need to handle them.

```

*****
CORIOLIS RESONANCES                               WI = WJ
*****

```

	I	J	WI	WJ	DIFF	ZETA	DeltaALPHA
ALPHA	3C	2	679.87	774.88	-95.01	-1.000	-0.00458
ALPHA	4C	1	647.70	805.41	-157.71	-0.351	-0.00034
ALPHA	5C	4	524.33	647.70	-123.37	-0.936	-0.00311

Figure: Coriolis resonances in spectro.out

Spectro

spectro.in again

The way I read these are the first number, then the second, then the letter. So 3, 2, C in the case of the first one here.

```

*****
CORIOLIS RESONANCES                               WI = WJ
*****
      I      J      WI      WJ      DIFF      ZETA      DeltaALPHA
ALPHA  3C    2    679.87    774.88    -95.01    -1.000    -0.00458
ALPHA  4C    1    647.70    805.41   -157.71    -0.351    -0.00034
ALPHA  5C    4    524.33    647.70   -123.37    -0.936    -0.00311
  
```

Figure: Coriolis resonances in spectro.out

Spectro

spectro.in again

And that's basically the way you put them in. The weirdest thing is that the letters are given by a vector. $A \rightarrow 1\ 0\ 0$, $B \rightarrow 0\ 1\ 0$, and $C \rightarrow 0\ 0\ 1$

```
# CORIOL #####
3
0
3 2 0 0 1
0
4 1 0 0 1
0
5 4 0 0 1
```

Figure: Coriolis resonances in spectro.in

Spectro

Rotational data

Spectro also outputs rotational constants, which can be found by searching:

- ▶ BZA - A , B , and C rotational constants for every vibrational state. BZA is usually A , BXA is B , and BYA is C . In this case we have A_0 , B_0 , and C_0 .

```
VIBRATIONAL STATE
NON-DEG(Vt) :      0      0      0      0      0      0

ROTATIONAL CONSTANTS (CM-1)
      BXA              BYA              BZA
      0.2148329       0.1295869       0.3275038
```

Spectro

Rotational data

Spectro also outputs rotational constants, which can be found by searching:

- ▶ DELTA, quartic distortion constants

	CM-1	MHz
DELTA J :	0.0000000702	0.0021030914
DELTA K :	0.0000002739	0.0082114140
DELTA JK :	-0.0000000477	-0.0014293852
delta J :	0.0000000271	0.0008129388
delta K :	0.0000000809	0.0024252037

Spectro

Rotational data

Spectro also outputs rotational constants, which can be found by searching:

- ▶ PHI, sextic distortion constants

	IN CM-1	IN Hz
PHI J :	0.6628031116D-13	0.1987033740D-02
PHI K :	0.1468897092D-11	0.4403642696D-01
PHI JK :	-0.2289305553D-12	-0.6863165389D-02
PHI KJ :	-0.7127345498D-12	-0.2136724426D-01
phi j :	0.3301218541D-13	0.9896804209D-03
phi jk :	-0.3351971470D-13	-0.1004895766D-02
phi k :	0.6056513421D-12	0.1815697045D-01

Reporting

Units and precision

- ▶ Vibrational frequencies to 1 decimal place in cm^{-1} , ex. 627.4 cm^{-1}
 - ▶ Harmonic frequencies are denoted ω_n (omega)
 - ▶ Anharmonic frequencies are denoted ν_n (nu)
- ▶ A , B , and C , rotational constants to 1 decimal place in MHz
- ▶ Δ and Φ constants to 3 decimal place but no more than 5 sig figs. Adjust units accordingly. For example, instead of 35154.123 kHz, use 35.154 MHz
- ▶ Bond lengths to 5 decimal places
- ▶ Bond angles (I think) to 3 decimal places

Reporting

Mode descriptions

Given symmetry internal coordinates, S_n , like those on the left, which go in the Computational Details, we often want to describe the resulting vibrational modes as linear combinations of them, as on the right

$$S_1(a_1) = r(H_1 - C_1) \quad (1)$$

$$S_2(a_1) = r(H_1 - C_2) \quad (2)$$

$$S_3(a_1) = \frac{1}{\sqrt{2}}[r(C_2 - C_3) + r(C_2 - C_4)] \quad (3)$$

$$S_4(a_1) = \frac{1}{\sqrt{2}}[r(C_3 - H_2) + r(C_4 - H_3)] \quad (4)$$

Mode	Description	Symmetry
ω_1	$0.96S_1$	a_1
ω_2	$0.95S_4$	a_1
ω_3	$1.00S_8$	b_2
ω_4	$0.68S_2 + 0.28S_3$	a_1
ω_5	$0.74S_5 + 0.24S_2$	a_1
ω_6	$0.90S_{10} + 0.12S_9$	b_2
ω_7	$0.58S_{11} + 0.31S_9 + 0.09S_{10}$	b_2

Reporting

Mode descriptions

Fortunately, you can find this information by searching “ASSIGNMENT” in intder.out

```
VIBRATIONAL ASSIGNMENTS
```

MODE	CM-1	DOMINANT COMPONENTS OF TED	
1	302.0	4 (100.0)	
2	524.3	2 (95.2)	-1 (4.8)
3	647.7	3 (100.0)	
4	679.9	6 (100.0)	
5	774.9	5 (100.0)	
6	805.4	1 (95.2)	2 (4.8)

In this case, basically every frequency lines up 1:1 with a symmetry internal coordinate, but as shown on the previous slide this is not always the case